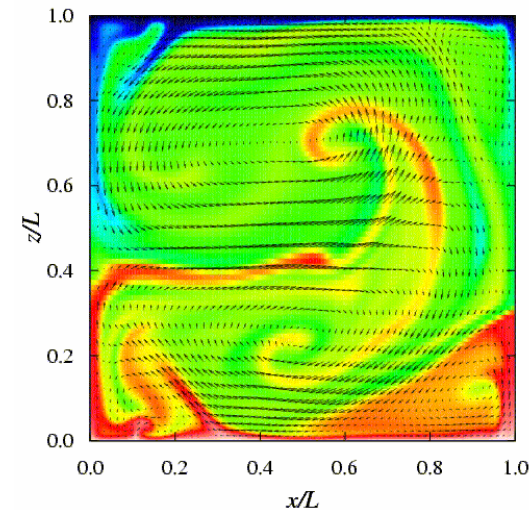


Flow organization in highly turbulent thermal convection



by



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Ladies and Gentlemen,
dear colleagues and friends,

it is with my greatest pleasure to address our Nestor
and always stimulating academic advisor,
Professor Hermann Haken,
with my sincerest congratulations
on the occasion of his 85th birthday.

I wish to express my
warmest thanks and appreciation
for his leadership and his guidance

Thank you, Hermann,
for being our ideal over all the years,
Kindly accept all my best wishes for you!

The results I want to present have been obtained
in close cooperation with the following
colleagues ... and more

Detlef Lohse, Enschede

Kazuyazu Sugiyama, Riken

Richard J. A. M. Stevens, Maryland

Roberto Verzicco, Roma

Guenter Ahlers, Santa Barbara

Eberhard Bodenschatz, Göttingen

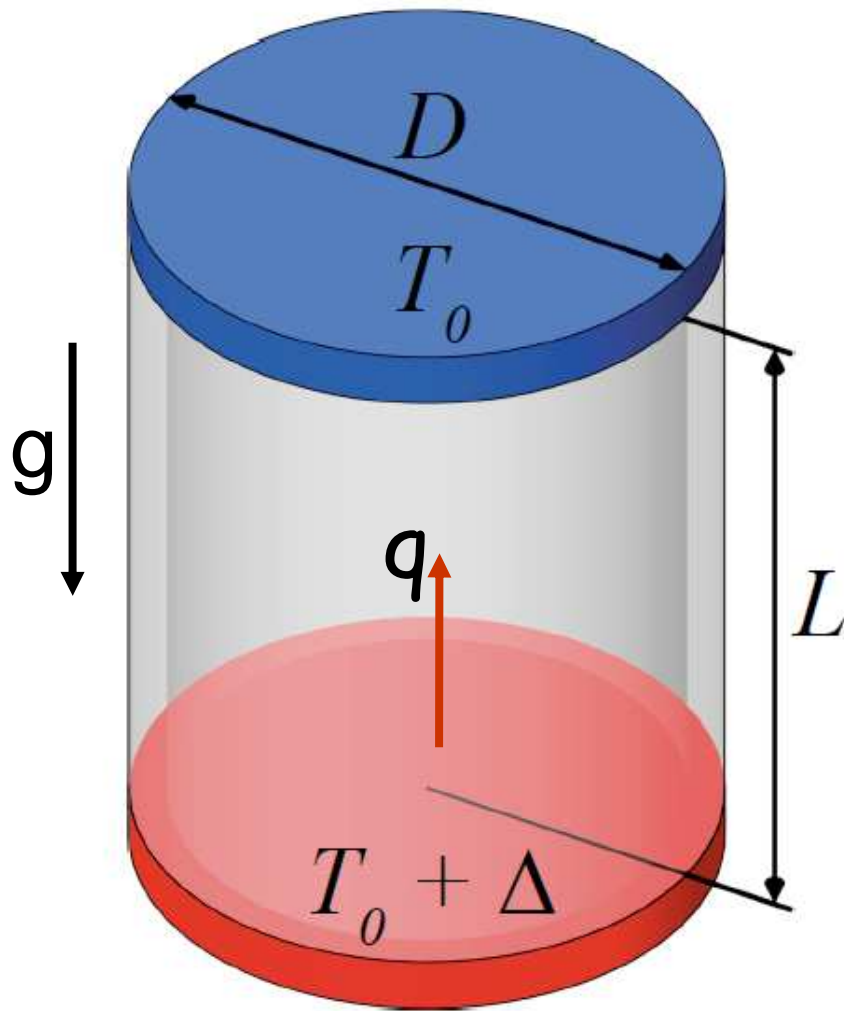
Denis Funfschilling, Nancy

Xiaozhou He, Göttingen

Ke-Qing Xia, Hong Kong

Quan Zhou, Shanghai

The Rayleigh-Bénard experiment



Control parameter:

$$Ra = \frac{\beta_p g L^3 \Delta}{\nu \kappa}$$

$$Pr = \nu / \kappa$$

Response:

$$Nu = q / \Delta L^{-1}$$

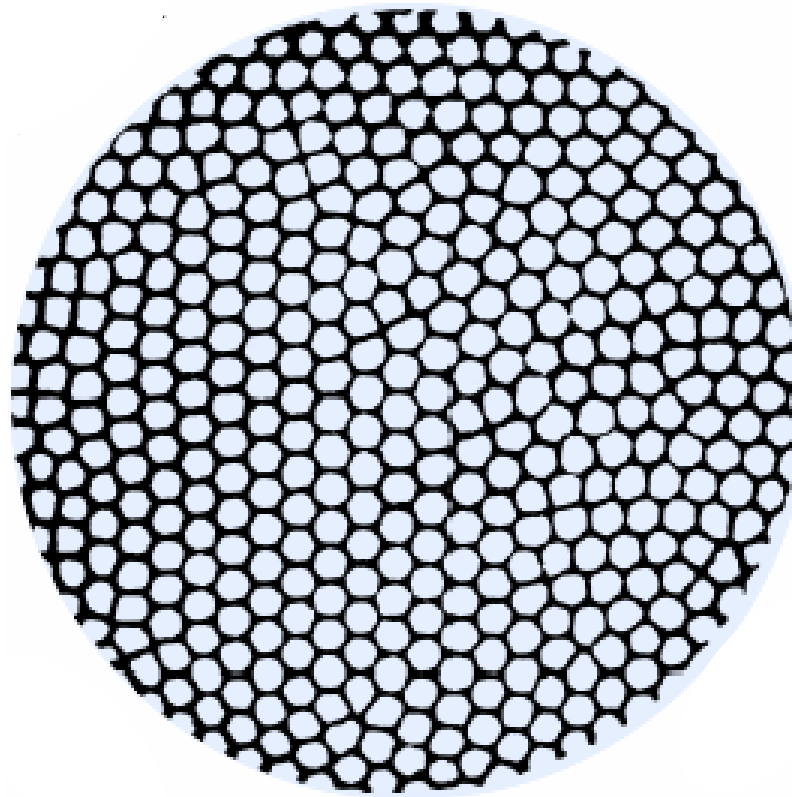
$$Re = U L / \nu$$

Pattern formation
in Bénard's historical experiment
Henri Bénard (1874 - 1939)
PhD thesis in Paris 1900

$$\Delta = 100^{\circ}\text{C} - 20^{\circ}\text{C}$$
$$= 80\text{K}$$

$$L = 0.81 \text{ mm}$$

$$\text{Ra} \approx 1000$$
$$\text{to } 2000$$

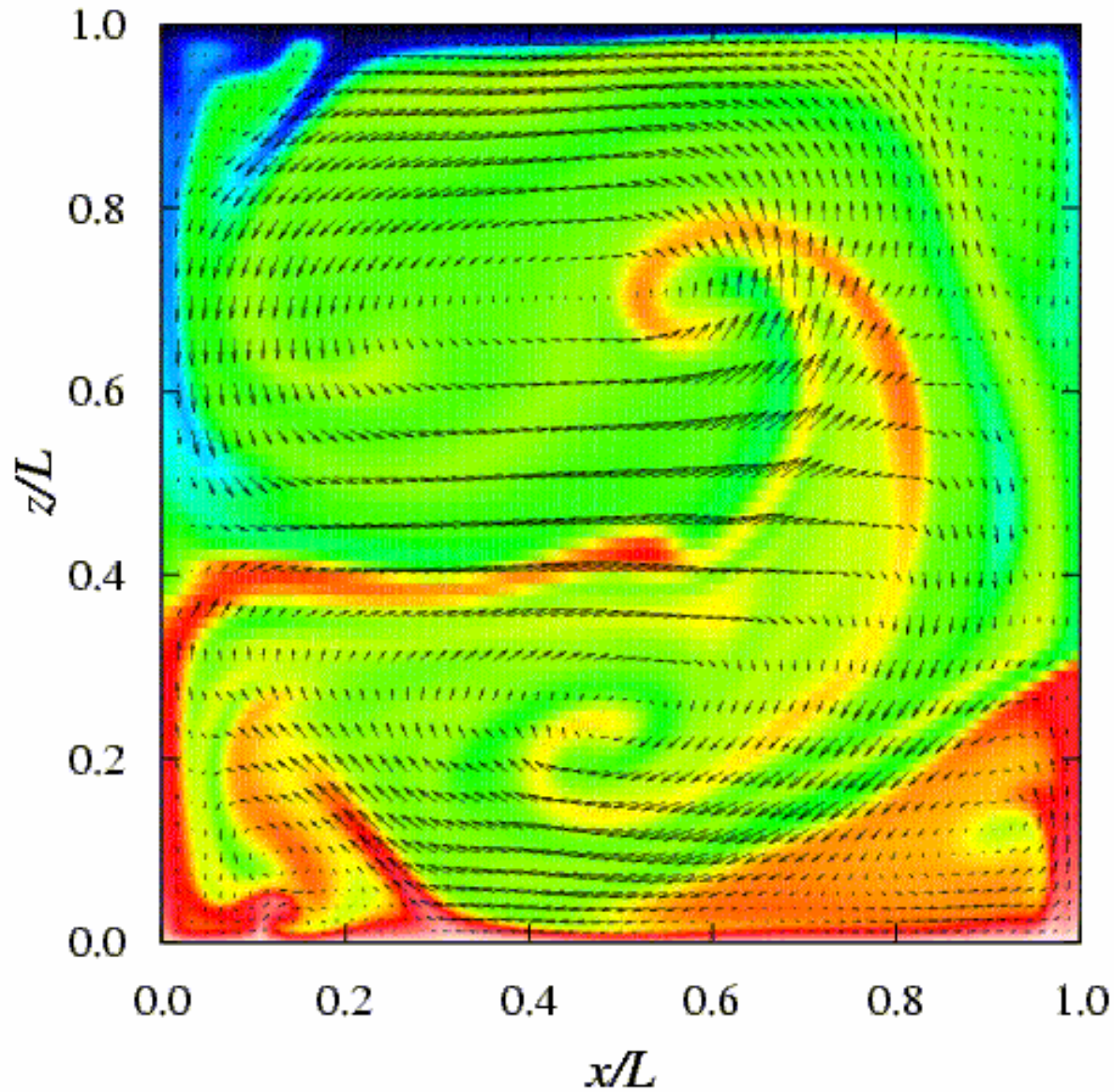


• Kaz Sugiyama, E. Calzavarini, S. G. N. D. Lohse, JFM 637 (2009) 105, Flow organization ...

• Same authors: ETC12 (2009) 479 Flow amplitudes

• Sugiyama, Ni, Stevens, Chen, Zhou, Sun, S. G. N. Xia, Lohse, PRL 105 (2010) 034503
Flow reversals

Snapshot of the flow and thermal field



2dim DNS

$Ra = 10^8$

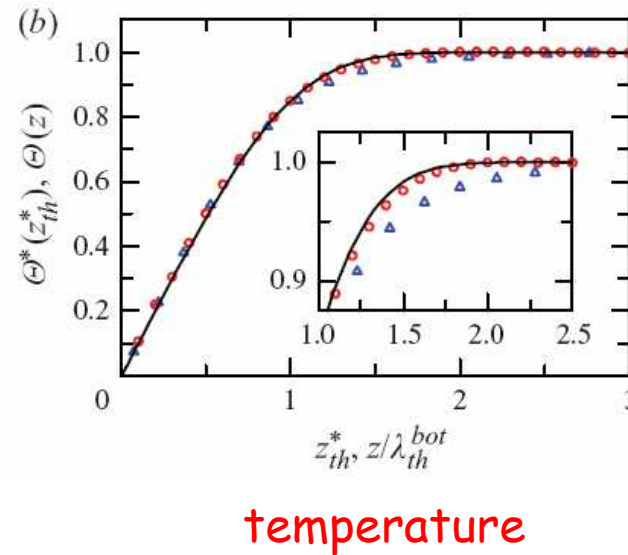
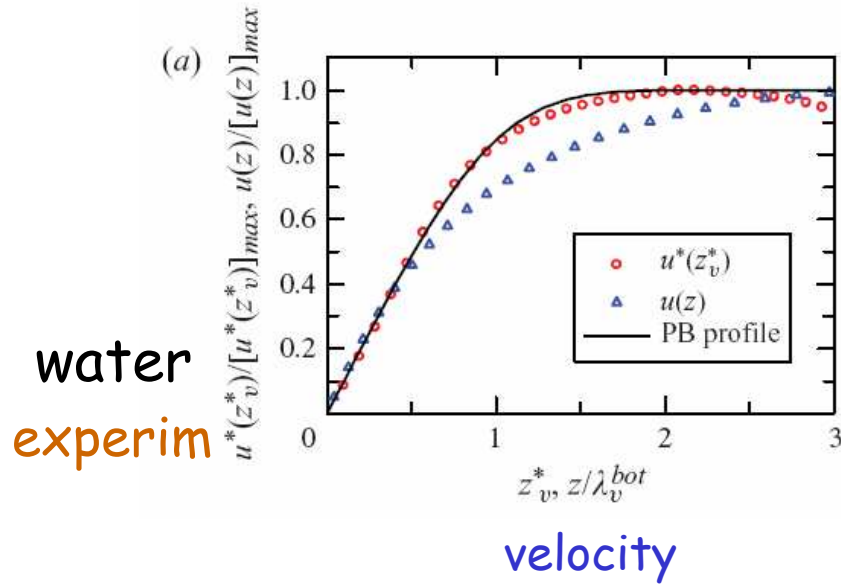
$Pr = 4.3$

$\Delta = 40 \text{ K}$

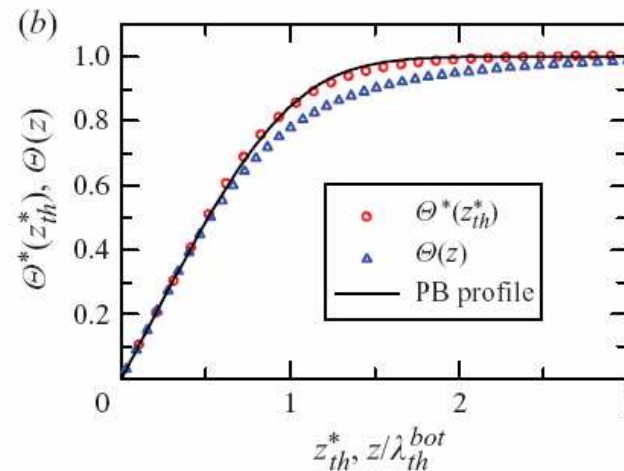
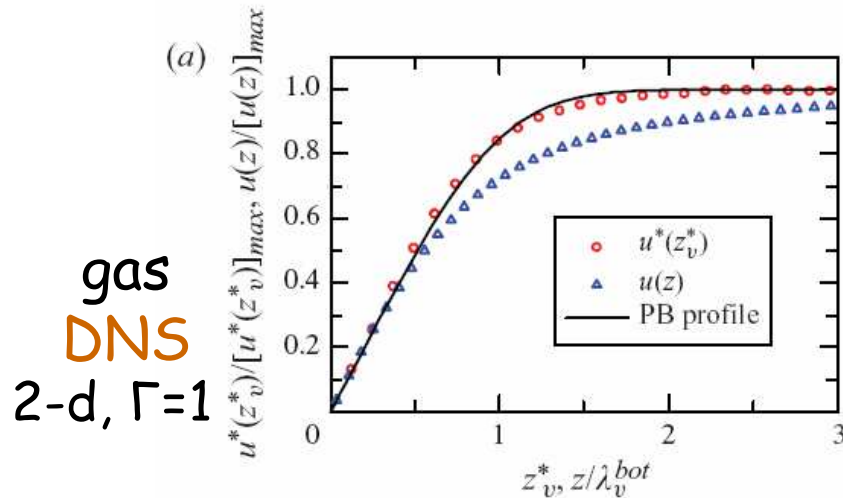
$Nu \approx 26$

$Re \approx 1000$

Experimental and numerical verification of Prandtl-Blasius profile, if dynamically rescaled

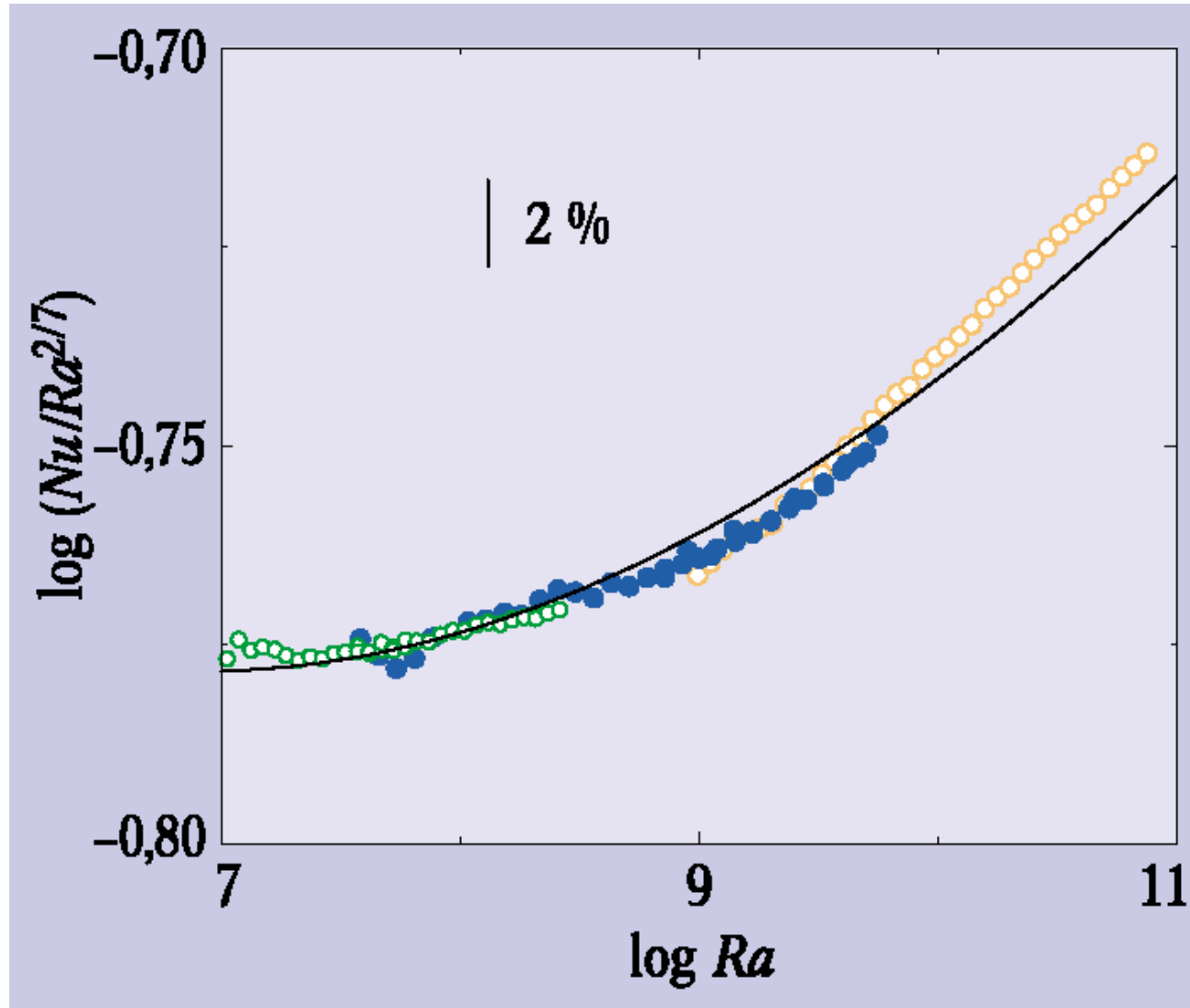


$Ra = 10^8$
 $Pr = 4.3$
 water
 experiment



$Ra = 10^9$
 $Pr = 0.7$
 gas
 DNS

Nu(Ra)



Theoretical prediction
GL 2000 etc:
no power law!

Experimental confirmation that there is no power law in Nu(Ra)

Ahlers et al.,
PRL2001

Why do the scaling exponents depend on Ra, Pr ?

Decompose central non-equilibrium quantity into bulk and BL parts!

dissipation rate $\tilde{\epsilon}_u = \frac{\epsilon_u}{\nu^3 L^{-4}} = Pr^{-2} Ra (Nu - 1)$

▶ $\tilde{\epsilon}_u =$ BL-part + bulk-part

▶ $\tilde{\epsilon}_u = \sim \nu (U/\delta)^2 \cdot \delta/L + \sim U^3/L$

take Prandtl's law for BL width: $\delta/L = a/\sqrt{Re} \rightarrow$ BL part $\sim Re^{5/2}$

thermal flux $J = \kappa \Delta L^{-1} Nu = -\kappa \partial_3 \langle \theta \rangle_{A,t} + \langle u_3 \theta \rangle_{A,t}$

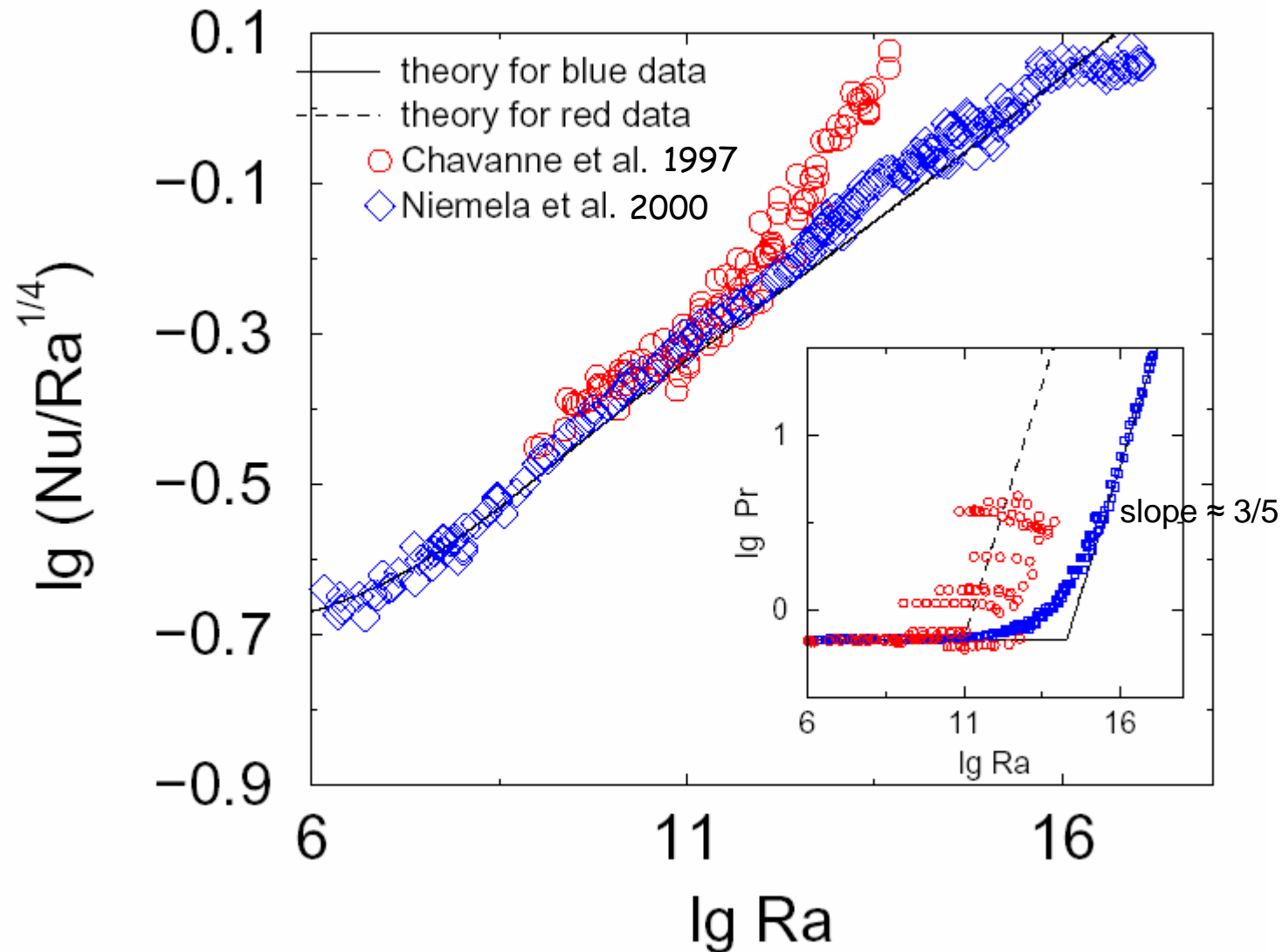
▶ $Nu =$ BL-part + bulk-part

▶ $Nu = \sim \frac{L}{\lambda} + \sim \frac{U}{\kappa L^{-1}}$

BL eq. $UL^{-1} \sim \kappa \lambda^{-2}$ ▶ $Nu = \sim \sqrt{Pr Re} + \sim Pr Re$

Pohlhausen $Re-Pr$ -dependence ; "lower" or "upper" cases: U or $U \cdot \lambda/\delta$

The ultimate range mystery



Grenoble: Chavanne et al., PRL 79 (1997) 3648 and PoF 13 (2001) 1300

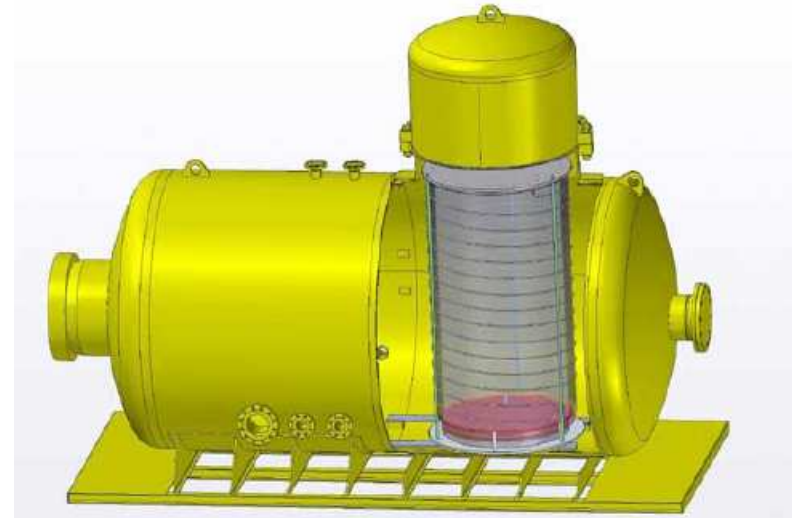
Oregon: Niemela et al., Nature 404 (2000) 837; J.Low.Temp.Phys.143(2006)163

"High pressure convection facility"



The Göttingen U-Boot, MPI DSO
RB-facility: $M_{\text{tot}} = 2\,000\text{ kg}$

G.Ahlers, D.Funfschilling,
E. Bodenschatz,
NJP 11 (2009) 123001

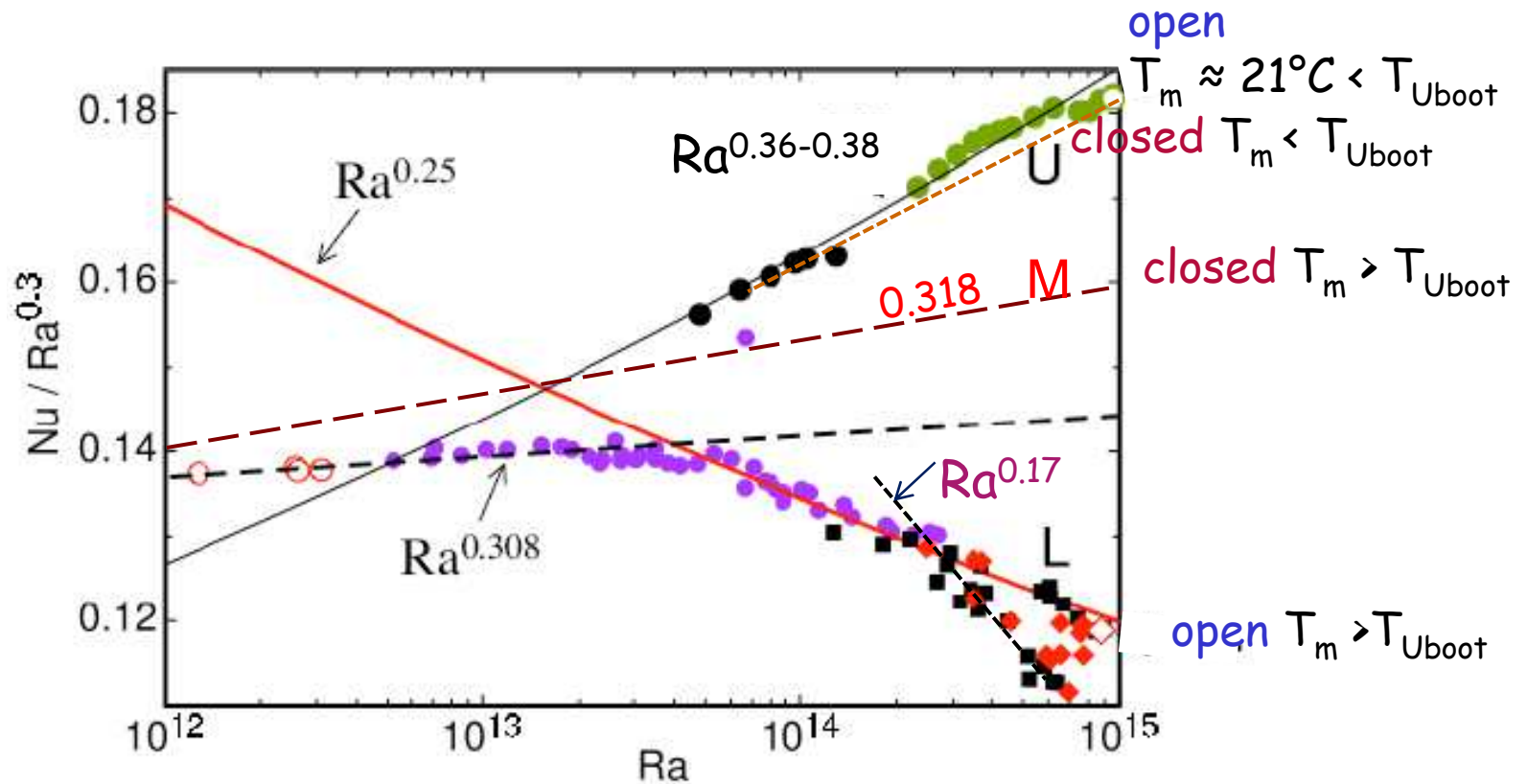


height $L = 2.24\text{ m}$
diameter $D = 1.12\text{ m}$, $\Gamma = 0.5$
(He, Air) N_2 ; SF_6 , $Pr \approx 0.86$
pressure p up to 19 bar,
 $T_m \approx 25^\circ\text{C}$, $\Delta T \approx 10 - 12\text{ K}$

$Ra \approx 10^{15}$, $Nu \approx 5000$, $Re \approx 10^6$

$\lambda/L \approx 10^{-4}$, $\lambda_{\text{Uboot}} \approx 0.22\text{ mm}$
 $\delta/L \approx 5 \times 10^{-4}$, $\delta_{\text{Uboot}} \approx 1.12\text{ mm}$

Several ultimate range states



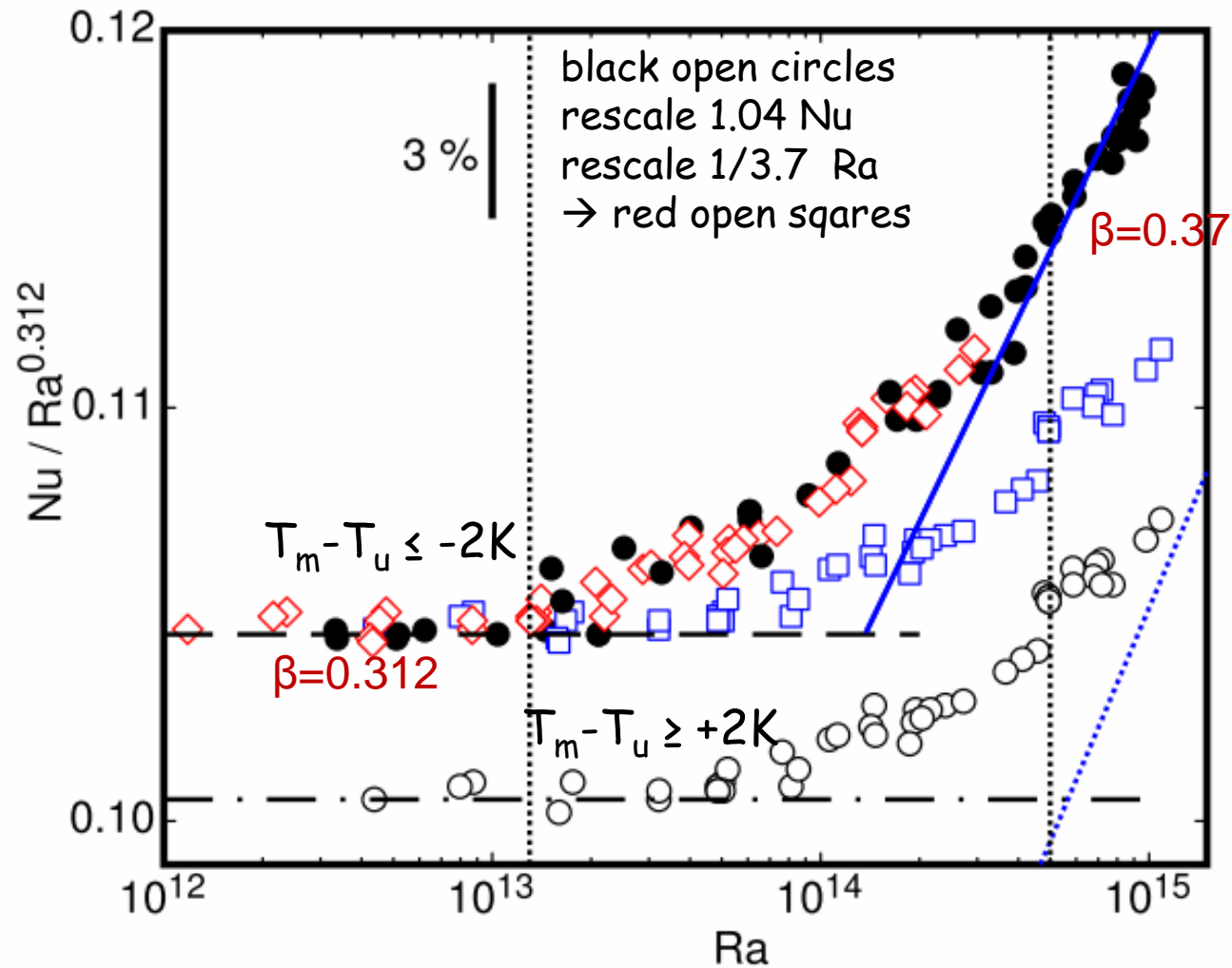
and even more, depending on ambient temperature, $T_m \neq T_{Uboot}$

G. Ahlers, D. Funfschilling, E. Bodenschatz,
Ahlers-talk at Les Houches workshop, Jan 27, 2010

www.hirac4.cnrs.fr/HIRAC4_Talks_files/Ahlers.pdf and NJP 13(2011)049401

Heat transport by turbulent RB convection, $Pr=0.8, \Gamma=1/2$
G. Ahlers, X.-Z. He, D. Funfschilling, E. Bodenschatz, NJP, 2012

Fig.5, page 15



Laminar \rightarrow turbulent transition in BL

$$\text{if } Re_s = \frac{U\delta}{\nu} = a\sqrt{Re} \text{ large enough}$$

turbulent if Re_s exceeds $Re_s^* = 420$; others: 320 - 150

$\rightarrow Re^* = (Re_s^*/a)^2$ exceeds 7.1×10^5 ; or $(4.1 - 0.9) \times 10^5$

The "wind" (in region IV_u) is $Re \approx 0.346 Ra^{4/9} Pr^{-2/3}$

\rightarrow Transition expected at $Re^* = A Pr^{3/2}$

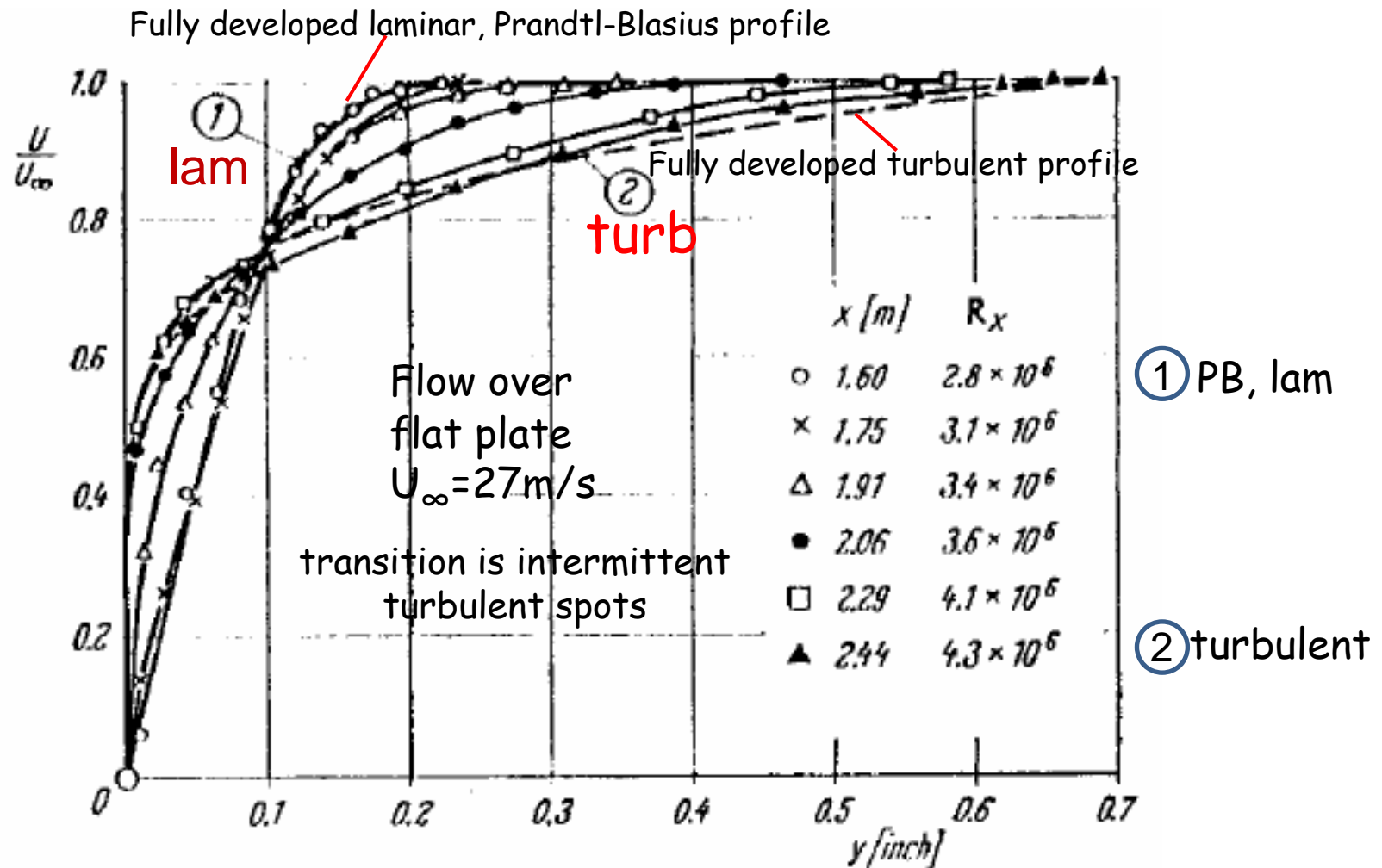
for $Pr = 0.86$ transition near $Re^* = 1.25 \times 10^{14}$;

or $= 3.7 \times 10^{13}$ to 1.22×10^{12}

Prandtl BL thickness $\delta^*/L = a/\sqrt{Re^*} = O(6 \times 10^{-4}) \dots O(8 \times 10^{-4})$

i. e. in U-Boot: $\delta^* = 1.3 \text{ mm}$ or 1.8 mm or 3.7 mm - $O(17 \times 10^{-4})$

Velocity profiles at laminar-turbulence transition



Turbulent BL MUCH steeper and MUCH thicker than laminar BL

G.B.Schubauer and P.S.Klebanoff, NACA TN 3489(1955)

Aus: Hermann Schlichting, BL Theory, 7th Edition, 1979, p. 454, Fig.16.4

The *key quantity* in turbulent U-driven flows is the fluctuation scale u_*

Represents the shear stress or drag at the wall:

$$u_*^2 = \sigma_{xz}(0) = p_{xz}(0)/\rho = \nu U_{x|z}(0) \sim \text{slope of profile}$$

$$\frac{u_*^2}{U^2} \text{ wall friction coefficient; } u_* \text{ determines } \nu_{turb} = \bar{\kappa} u_* z, \kappa_{turb}$$
$$u_* \text{ determines local turbulent dissipation rate } \varepsilon_u(z) = \frac{u_*^3}{\bar{\kappa} z}$$

PoF23,045108(2011):

$$\frac{u_*}{U} = \frac{\bar{\kappa}}{\ln\left(Re \frac{u_*}{U} \frac{1}{b}\right)} = \bar{\kappa} F\left(\frac{\bar{\kappa}}{b} Re\right), \text{ continued fraction solution}$$

b empirical constant, $b = e^{-\bar{\kappa} B_u}$

Linear viscous sub-layer near wall; $z_* = \nu/u_*$, followed by buffer range, then log-profile; $\delta_{\log} = O(L)$, i.e., the turbulent „BL“ occupies full bulk!

for $Re \approx 6 \times 10^5$ it is $z_*/L = 0.5 \times 10^{-4}$ instead of $\delta / L = 6.45 \times 10^{-4}$

U-Boot: $z_* \approx 0.11$ mm, while $\delta \approx 1.45$ mm and $\delta_{\log} \approx 1$ m

Scaling

in the three ultimate states

(effective, local exponents)

$$(a_1) \text{ u-log-turb, } \theta\text{-lam,plume} \quad \text{Nu} \sim \text{Ra}^{0.14} \text{Pr}^{0.10}$$

$$\text{Re} \sim \text{Ra}^{0.41} \text{Pr}^{-0.69}$$

$$(a_2) \text{ u-log-turb, } \theta\text{-lam,fluct} \quad \text{Nu} \sim \text{Ra}^{0.23} \text{Pr}^{0.16}$$

$$\text{Re} \sim \text{Ra}^{0.45} \text{Pr}^{-0.68}$$

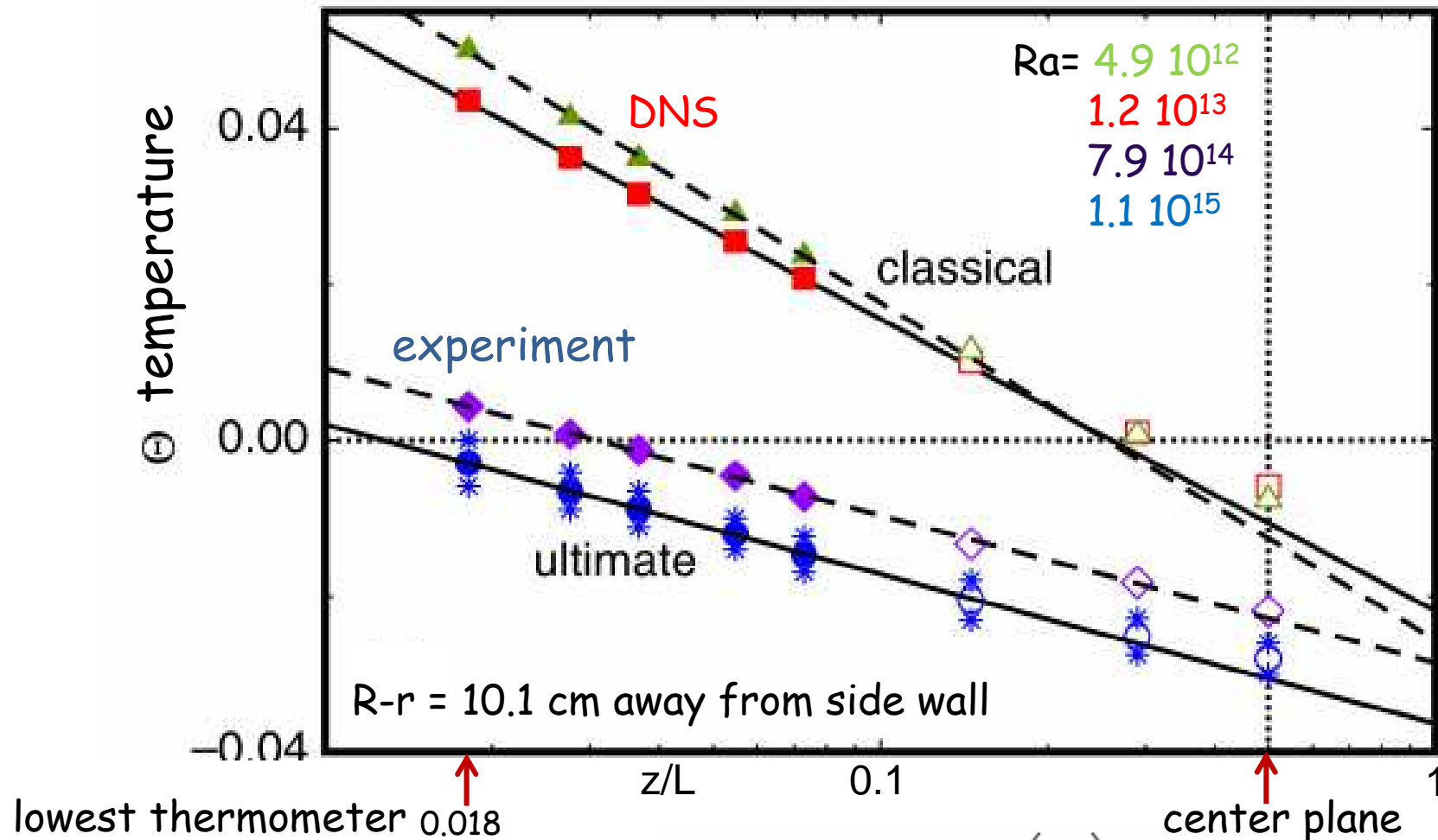
$$(b) \text{ u-log-turb, } \theta\text{-log-turb} \quad \text{Nu} \sim \text{Ra}^{0.38} \text{Pr}^{0.64}$$

$$\text{Re} \sim \text{Ra}^{0.50} \text{Pr}^{-0.50}$$

- Predictive features of theory: i) Nu- and Pr-exponents differ in all states,
ii) Nu- and Pr-exponents depend on Ra !, iii) thermal and velocity BL profiles differ
iv) In double-turbulent state Re has **NO** log-correction!

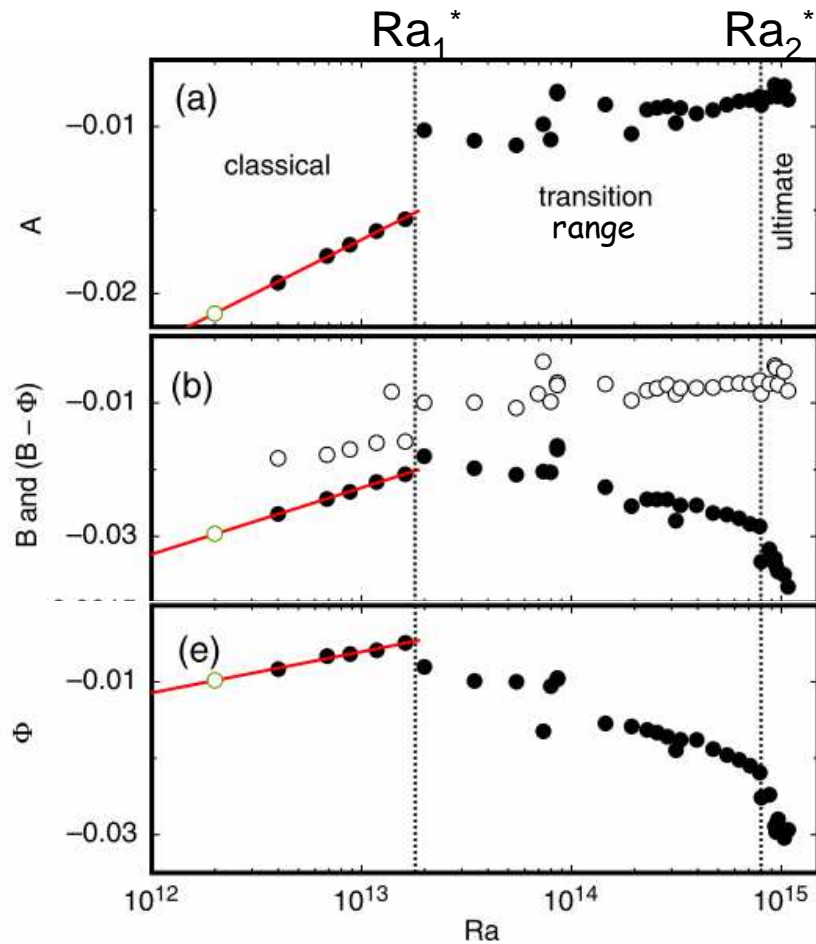
"Law of the wall" - log-profile!

ABFGHLSV. Phys. Rev. Lett. 109(2012)114501



$$(\langle T(z) \rangle - T_m) / \Delta = \Theta(z) = A \cdot \ln \left(\frac{z}{L} \right) + B$$

The profile parameters



Theory for ultimate state:

$$A \sim Ra^{-0.043},$$

very weak decrease with Ra

$B - \Phi$ should correspond to B if OB

$$A = -\frac{\kappa Nu}{\bar{\kappa}_\theta L u_*} \approx -\frac{1}{2\bar{\kappa}} \frac{u_*}{U} \approx -0.038$$

$$B = \ln 2 \cdot A \approx -0.026$$

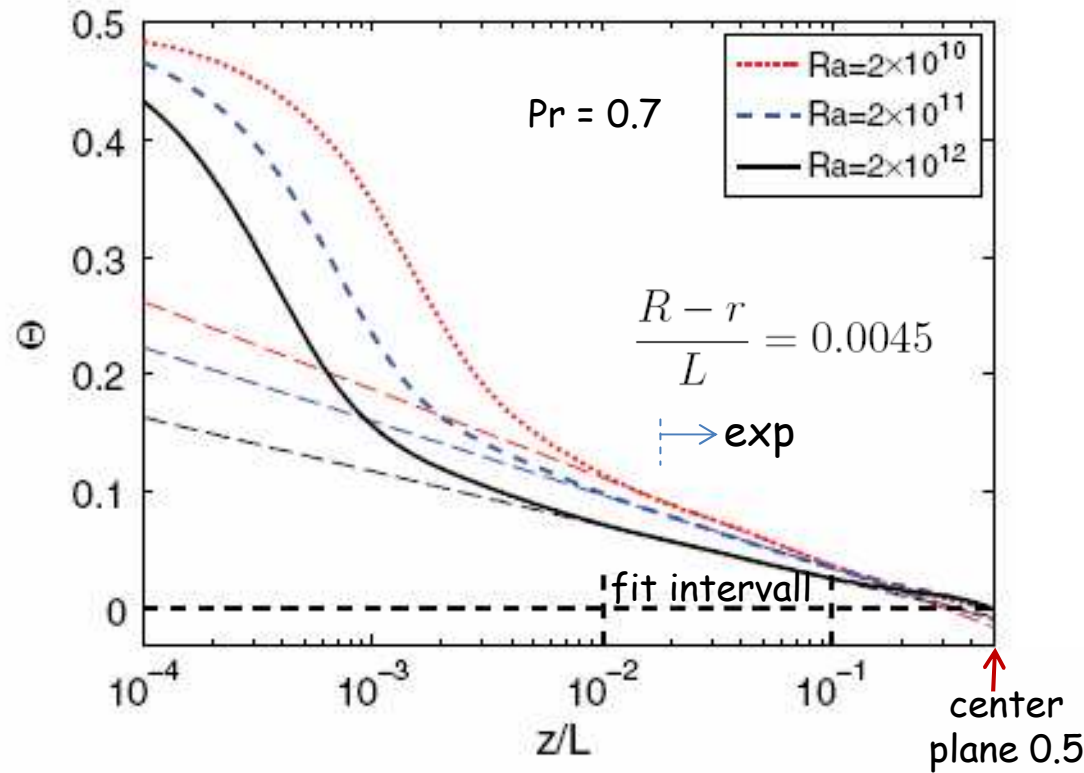
$\approx 70\%$ less

Φ nonzero
probably due to yet
unknown NOB effects?

DNS

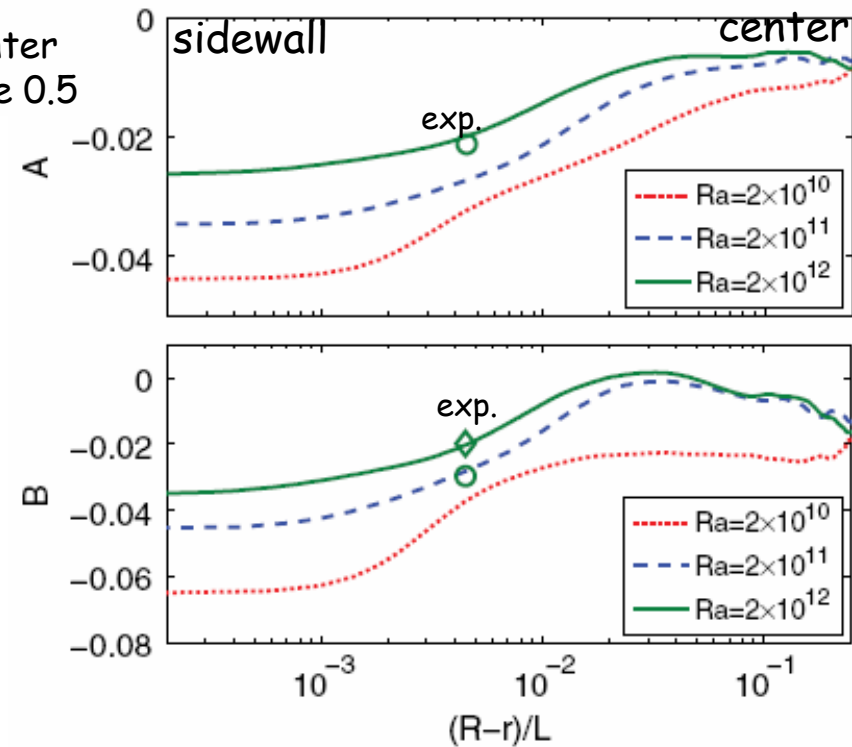
side wall distance 10.1 cm

$|A(r)|$ increases with distance r from center



time and azimuthally averaged
top and bottom profile averaged

excellent agreement
of DNS with data



The logarithmic temperature profile

$$\partial_t T = -\vec{u} \cdot \vec{\nabla} T + \kappa \Delta T, \quad T(z=0) = 0, T(z=L) = -\Delta$$

$$0 = -\vec{U} \cdot \vec{\nabla} \Theta - \overline{\vec{u}' \cdot \vec{\nabla} \theta'} + \kappa \Delta \Theta$$

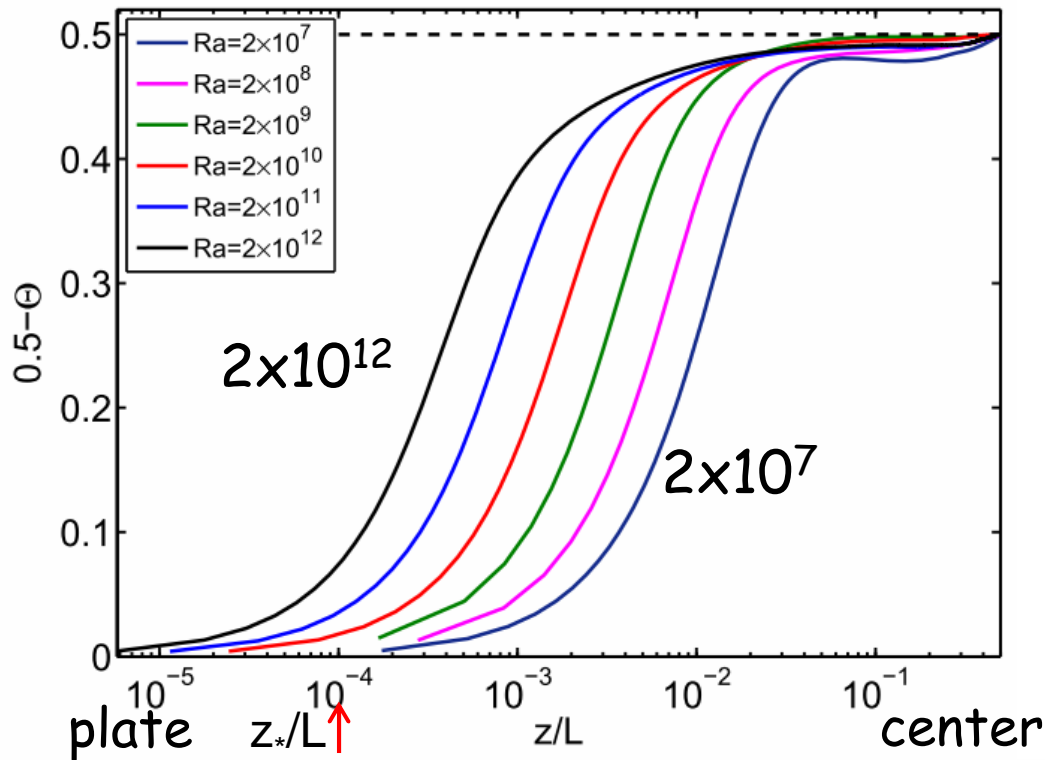
Reynolds & mixing length ansatz: $\overline{\vec{u}' \theta'} \approx -\kappa_{turb}(z) \partial_z \Theta$

$$(\kappa_{turb}(z) + \kappa) \partial_z \Theta(z) = \kappa \partial_z \Theta(0) \equiv J \quad \text{or} \quad Nu \cdot \kappa \Delta / L$$

$$\kappa \gg \kappa_{turb} = \bar{\kappa}_\theta z u_* \quad \text{linear sublayer} \quad 0 \leq z \leq Pr^{-1} z_* / \bar{\kappa}_\theta$$

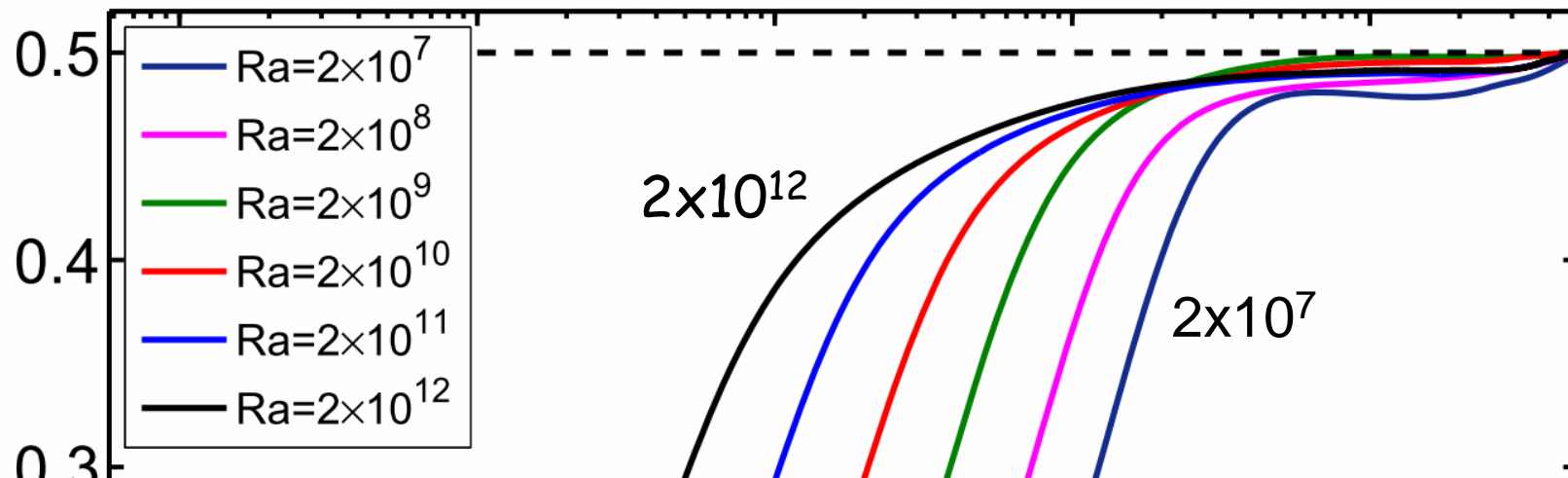
$$\kappa \ll \kappa_{turb} \quad \text{"law of the wall"} \quad \Theta(z) = -\frac{J}{\bar{\kappa}_\theta u_*} \left(\ln\left(\frac{z}{z_*}\right) + f(Pr) \right)$$

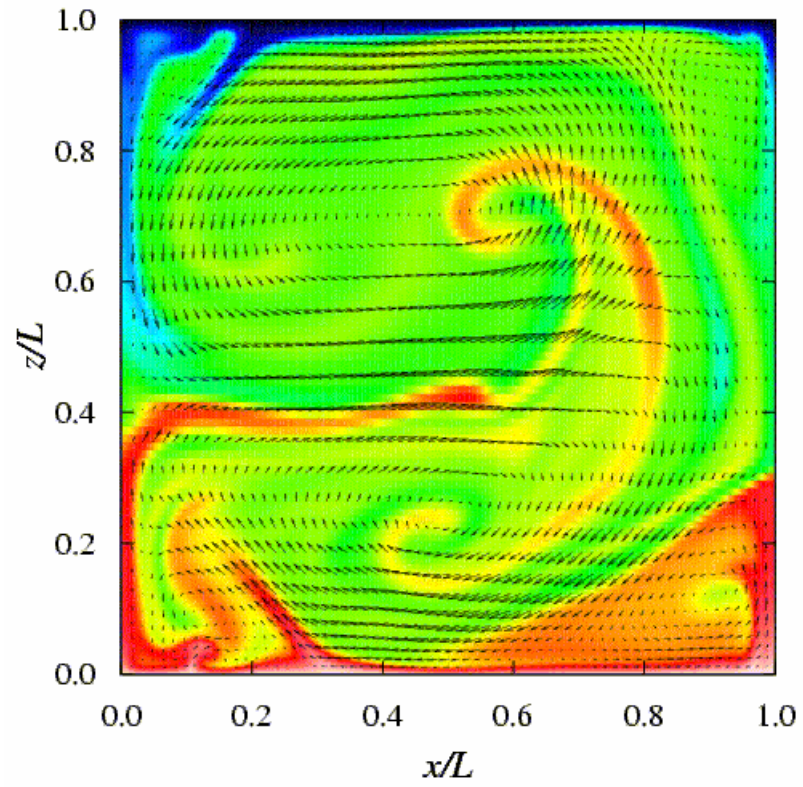
$$A = -\frac{\kappa Nu}{\bar{\kappa}_\theta u_* L} \approx -\frac{1}{2\bar{\kappa}} \cdot \frac{u_*}{U} \quad B = \ln 2 \cdot A$$



Temperature profiles
 in units of Δ ,
 measured at
 wall distance $z/L=0.15$

Transition
 to log profile:
 beyond 10^9





Thank you



References:

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6. G. Ahlers, D. Funfschilling, E. Bodenschatz, Transitions in heat transport by turbulent convection, *New J. Phys.* 11, 123001 (2009)
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